

PERFORMANCE ASSESSMENT OF PLANETARY MISSIONS  
AS LAUNCHED FROM AN ORBITING SPACE STATION

PRESENTED BY

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TO

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AT

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## INTRODUCTION

## THE PLANETARY/SPACE STATION ISSUE

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WOULD DEVELOPMENT OF A LOW EARTH-ORBIT SPACE STATION  
ENABLE NEW PLANETARY EXPLORATION OPPORTUNITIES?.....

.....ALTERNATIVELY, WOULD THE EXISTENCE OF A LOW EARTH-  
ORBIT SPACE STATION AND ITS MANDATED USE ADVERSELY AFFECT  
PLANETARY EXPLORATION OPPORTUNITIES?

## APPROACH AND SCOPE OF ANALYSIS

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- DESCRIBE THE BASIC CHARACTERISTICS AND MANEUVER STRATEGIES FOR LAUNCHING PLANETARY MISSIONS FROM A SPACE STATION IN EARTH ORBIT.
  
- QUANTIFY THE "INHERENT" PROS AND CONS IN TERMS OF:
  - INJECTED MASS CAPABILITY OF SELECTED UPPER STAGES
  - PLANE CHANGE PENALTIES
  - LAUNCH TIMING PENALTIES
  
- COMPARE STATION-LAUNCHED AND STANDARD SHUTTLE-LAUNCHED PERFORMANCE FOR A WIDE RANGE OF PLANETARY MISSION OPPORTUNITIES OVER LAUNCH ENERGY AND INJECTED MASS SPACE.
  - MARS GEOCHEMICAL ORBITER (LOW ENERGY, MODERATE MASS)
  - MARS SAMPLE RETURN (LOW ENERGY, LARGE MASS)
  - MULTIPLE ASTEROID RENDEZVOUS (LOW ENERGY, LARGE MASS)
  - ANTEROS RENDEZVOUS (MODERATE ENERGY, MODERATE MASS)
  - MERCURY ORBITER (MODERATE ENERGY, LARGE MASS)
  - TITAN PROBE (HIGH ENERGY, SMALL MASS)
  - URANUS/NEPTUNE PROBES (HIGH ENERGY, MODERATE MASS)
  - SATURN ORBITER/PROBE (HIGH ENERGY, MODERATE MASS)
  - GANYMEDE ORBITER (HIGH ENERGY, MODERATE MASS)
  - COMET RENDEZVOUS (HIGH ENERGY, MODERATE MASS)

## GROUND RULES AND ASSUMPTIONS

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### RATIONALE

- STATION ORBIT PARAMETERS

|                |                  |
|----------------|------------------|
| ALTITUDE       | 200 NM, CIRCULAR |
| INCLINATION    | 28.3°            |
| NODAL POSITION | ANY AND ALL      |

MOST PROBABLE PLACEMENT WITH MAXIMUM UTILIZATION OF SHUTTLE CARGO CAPACITY; YIELDS CONSERVATIVE PLANETARY PERFORMANCE CONCLUSIONS

- UPPER STAGE SELECTION

IUS(II)  
WIDE BODY CENTAUR  
OTV (MSFC 18' OTV)  
STAR 48 AS NEEDED

SET HAS WELL-DEFINED PERFORMANCE PARAMETERS OVER A RANGE OF CAPABILITY; OTV ADDS OPPORTUNITY FOR EXTENDED DEPARTURE MANEUVERS AND REUSABILITY

- SPACECRAFT PROPULSION

EARTH-STORABLES  
SOLIDS

UTILIZES PRESENT PROPULSION TECHNOLOGY YIELDING CONSERVATIVE PERFORMANCE RESULTS

- STATION DEPARTURE

ON TIME (0<sup>d</sup> WINDOW)

COMPARABLE TO SHUTTLE UPPER-STAGE CRITERIA; PERFORMANCE CONSEQUENCE OF DEPARTURE DELAYS IS EXAMINED

## SPACE STATION PROS & CONS - QUALITATIVE ASSESSMENT

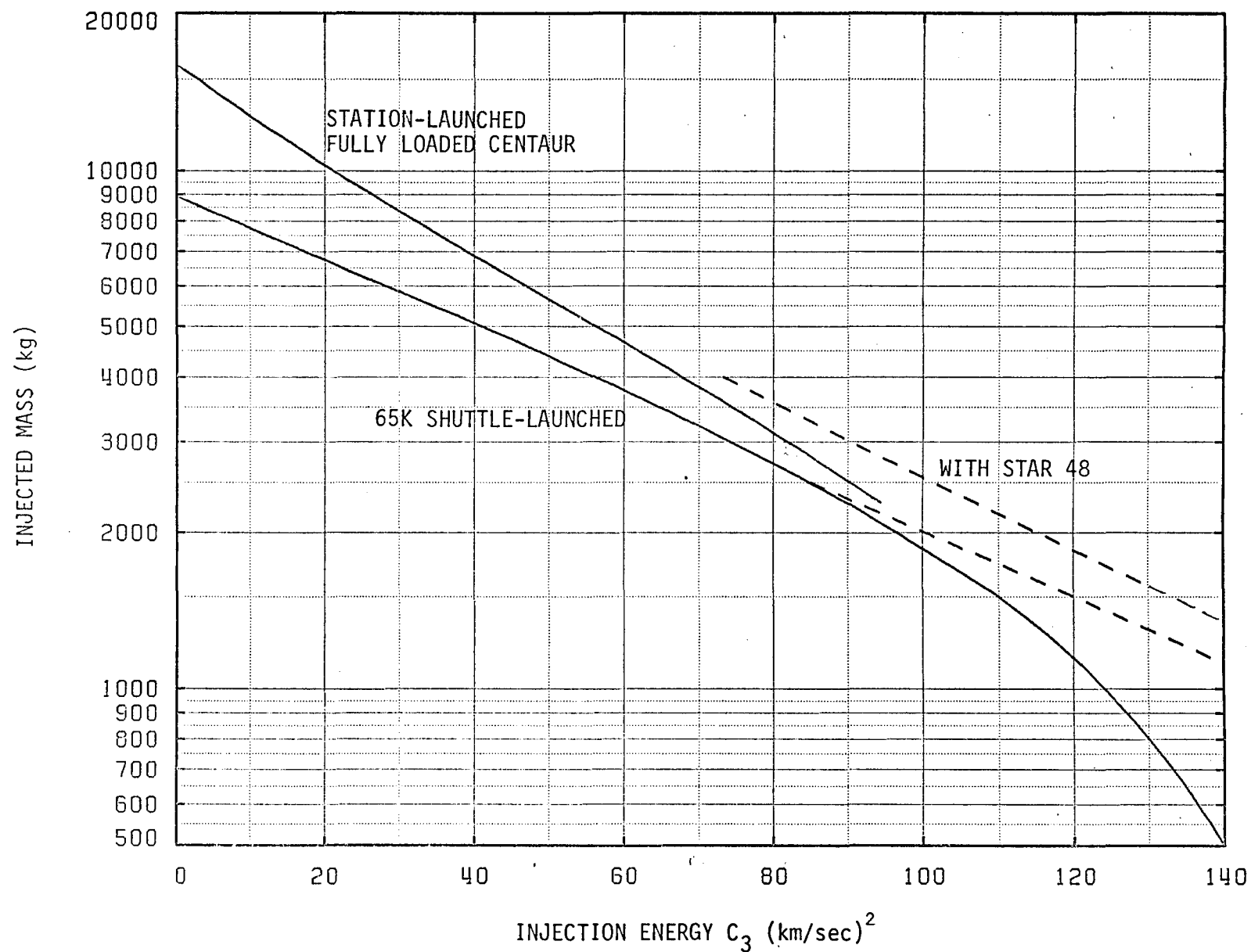
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### PROS

- MAXIMIZES SHUTTLE UTILIZATION
- ALLEVIATES SHUTTLE MANIFESTING THROUGH EARLY AND/OR FRACTIONAL LAUNCHES OF PAYLOAD
- ALLOWS FINAL CHECK-OUT AND ASSEMBLY IN SPACE ENVIRONMENT AFTER LAUNCH
- ASSURES FULLY LOADED STAGES
- POTENTIAL FOR "BEST-TIME" PLANETARY LAUNCHES (NO LAUNCH WINDOWS REQUIRED)
- ENHANCES REUSABLE STAGE OPTION

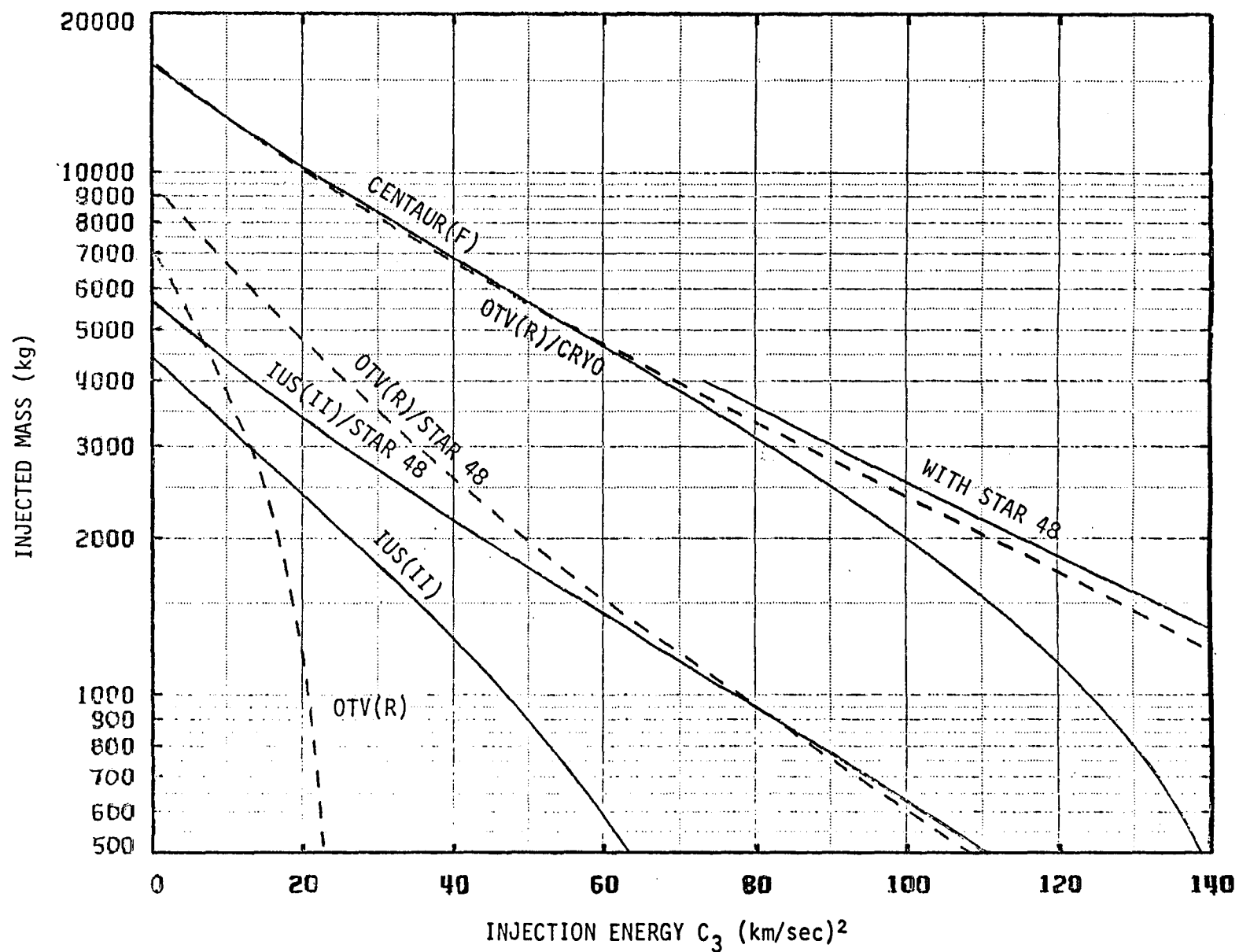
### CONS

- HIGH PROBABILITY OF MISSING OPTIMUM LAUNCH DATE DUE TO NODAL MISALIGNMENT
- HIGHER SENSITIVITY TO DLA-INCURRED PERFORMANCE PENALTIES
- MAXIMIZED PERFORMANCE IMPLIES MORE SHUTTLE LAUNCHES
- ADDED COST FOR ON-ORBIT PAYLOAD STORAGE, CHECK-OUT AND ASSEMBLY



WIDE BODY CENTAUR LAUNCH PERFORMANCE

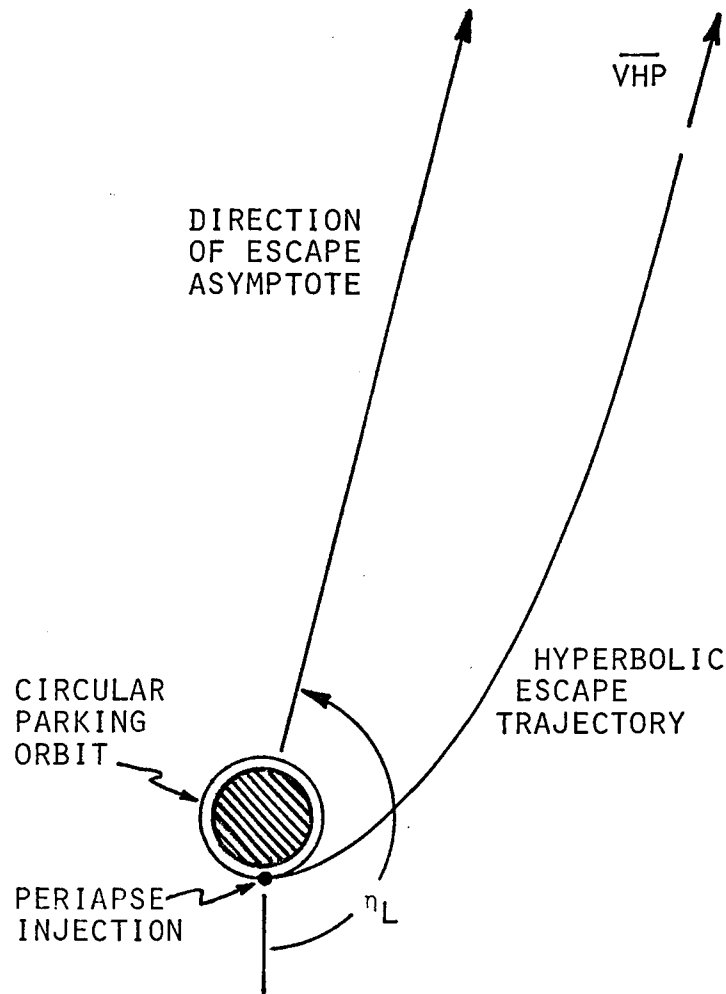




SPACE STATION-LAUNCHED UPPER STAGE PERFORMANCE

DESCRIPTION

# CHARACTERISTICS OF PLANETARY ESCAPE



$$C_3 = |\overline{VHP}|^2$$

$$\eta_L = \cos^{-1} \left[ \frac{-\mu}{\mu + R_p C_3} \right]$$

WHERE:  $\mu$  = EARTH'S GRAVITATIONAL PARAMETER

$R_p$  = PERIAPSE RADIUS

$C_3$  = VIS VIVA INJECTION ENERGY

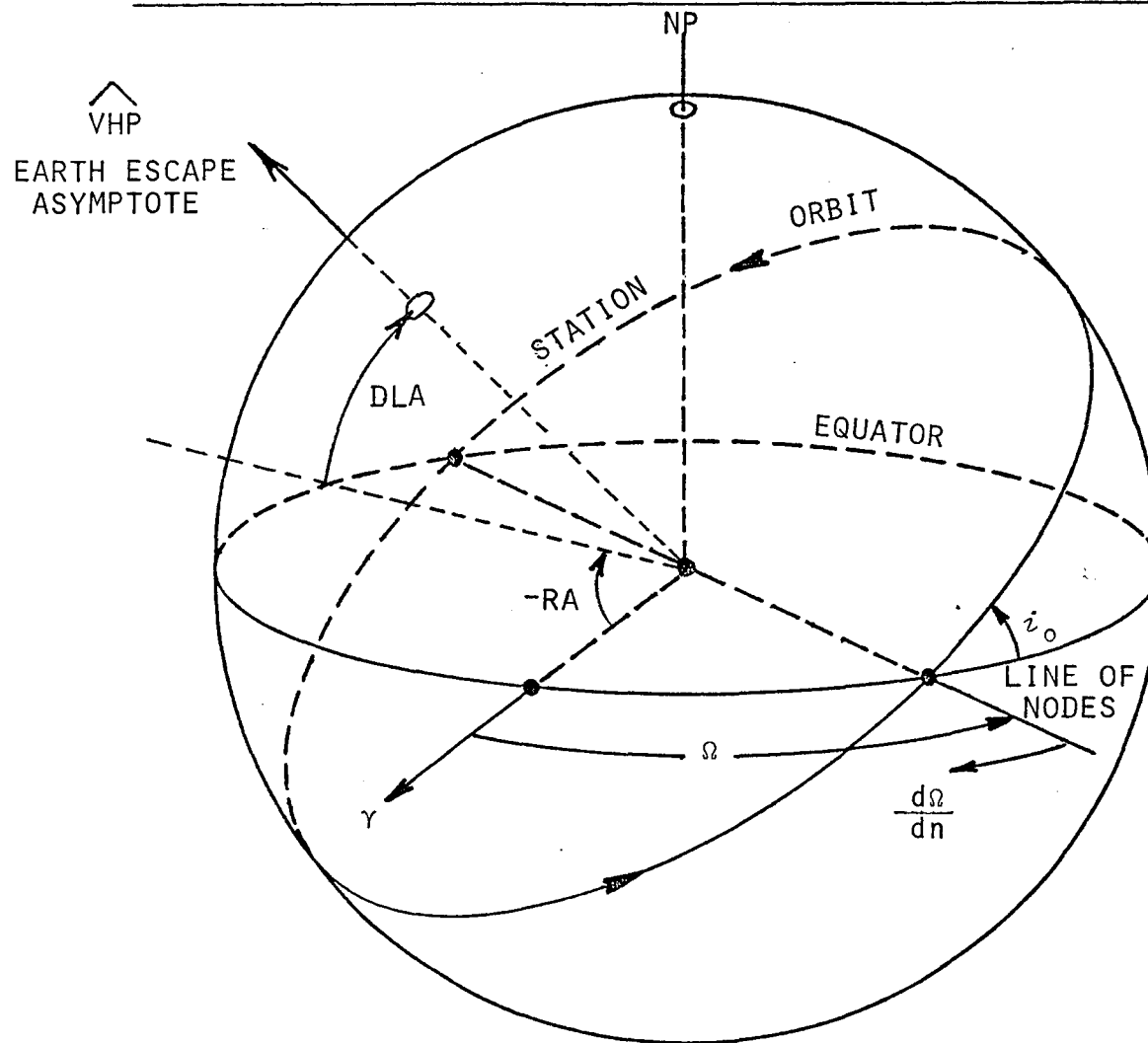
$\eta_L = 180^\circ$  WHEN  $C_3 = 0$  (PARABOLIC ESCAPE)

$\eta_L = 90^\circ$  WHEN  $C_3 = \infty$

$$E = \frac{mv^2}{2}$$

$$\frac{2E}{m} = v^2$$

# SPACE STATION ORBITAL GEOMETRY



## ORBIT PARAMETERS:

ALTITUDE,  $h = 200\text{nm}$  (CIRCULAR)

INCLINATION,  $i_0 = 28.3^\circ$

ASCENDING NODE,  $\Omega = \text{VARIABLE}$

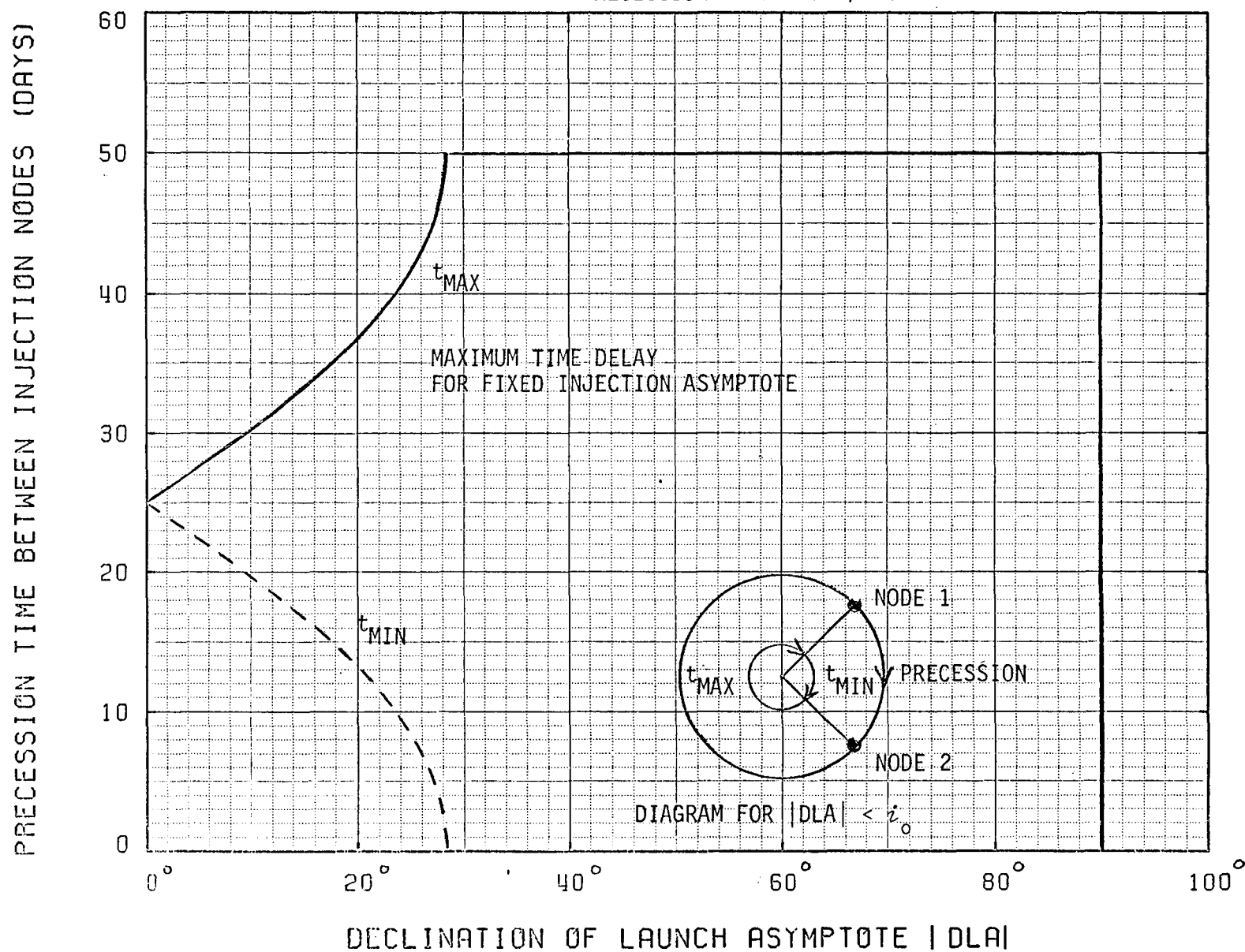
NODAL REGRESSION,  $\frac{d\Omega}{dt} = 0.46^\circ/\text{REV}$   
 $= 7.2^\circ/\text{DAY}$

## LAUNCHING PLANETARY MISSIONS FROM A SPACE STATION

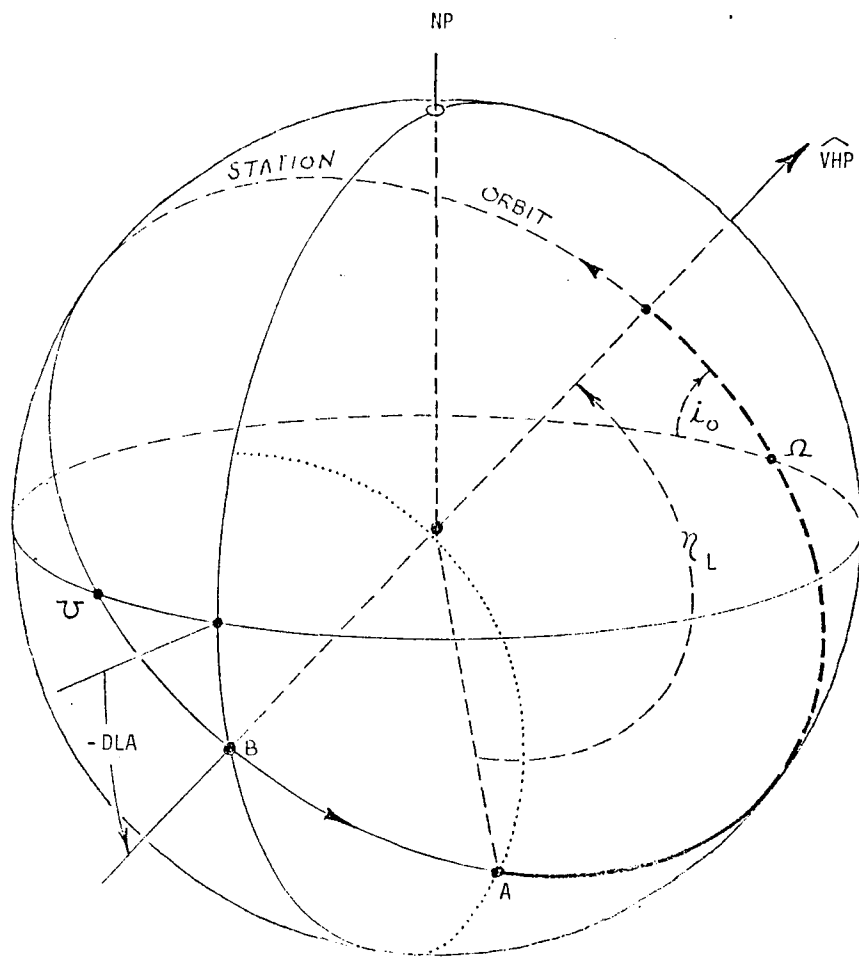
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- WHEN A PLANETARY MISSION OPPORTUNITY OCCURS, THE DIRECTION OF EARTH ESCAPE ( $\hat{VHP}$ ) IS RELATIVELY CONSTANT ACROSS THE LAUNCH WINDOW, WHICH TYPICALLY LAST 20 - 40 DAYS DEPENDING ON THE TARGET.
- CONVERSELY, THE STATION ORBIT PLANE IS CONSTANTLY PRECESSING DUE TO THE OBLATENESS OF THE EARTH; FOR THE ASSUMED ORBIT (200 NM CIRCULAR AT 28.3° INCLINATION) THE NODAL PRECESSION IS 7.2°/DAY IN THE OPPOSITE DIRECTION TO THE STATION'S ORBITAL MOTION.
- ASSUMING THE ANGLE (DECLINATION, DLA) OF  $\hat{VHP}$  TO THE EARTH'S EQUATOR IS LESS THAN THE ORBIT INCLINATION, THERE WILL, THEREFORE, BE ONLY TWO TIMES EVERY 50 DAYS ( $360^\circ/7.2$ ) WHEN  $\hat{VHP}$  LIES IN THE STATION ORBIT PLANE, WHICH IS THE CONDITION FOR OPTIMUM COPLANAR ESCAPE. AT ALL OTHER TIMES A PLANE CHANGE (AND PERFORMANCE LOSS) IS REQUIRED TO ACHIEVE THE CORRECT ESCAPE CONDITIONS.
- IF THE DECLINATION OF  $\hat{VHP}$  IS GREATER THAN THE ORBIT INCLINATION, AT NO TIME WILL  $\hat{VHP}$  BECOME COPLANAR WITH THE STATION ORBIT PLANE, AND ONLY ONCE EVERY 50 DAYS WILL IT COME CLOSEST TO THE PLANE MINIMIZING THE REQUIRED PLANE CHANGE (AND PERFORMANCE LOSSES).
- SINCE THESE CONDITIONS FOR OPTIMUM STATION DEPARTURE WILL NOT, IN GENERAL, COINCIDE WITH THE TIME OF MINIMUM  $C_3$  ( $C_3 = |\overline{VHP}|^2$ ) A TRADE-OFF EXISTS BETWEEN THE AMOUNT OF PLANE CHANGE REQUIRED AND THE  $C_3$  OF OFF-OPTIMAL LAUNCH DATES.

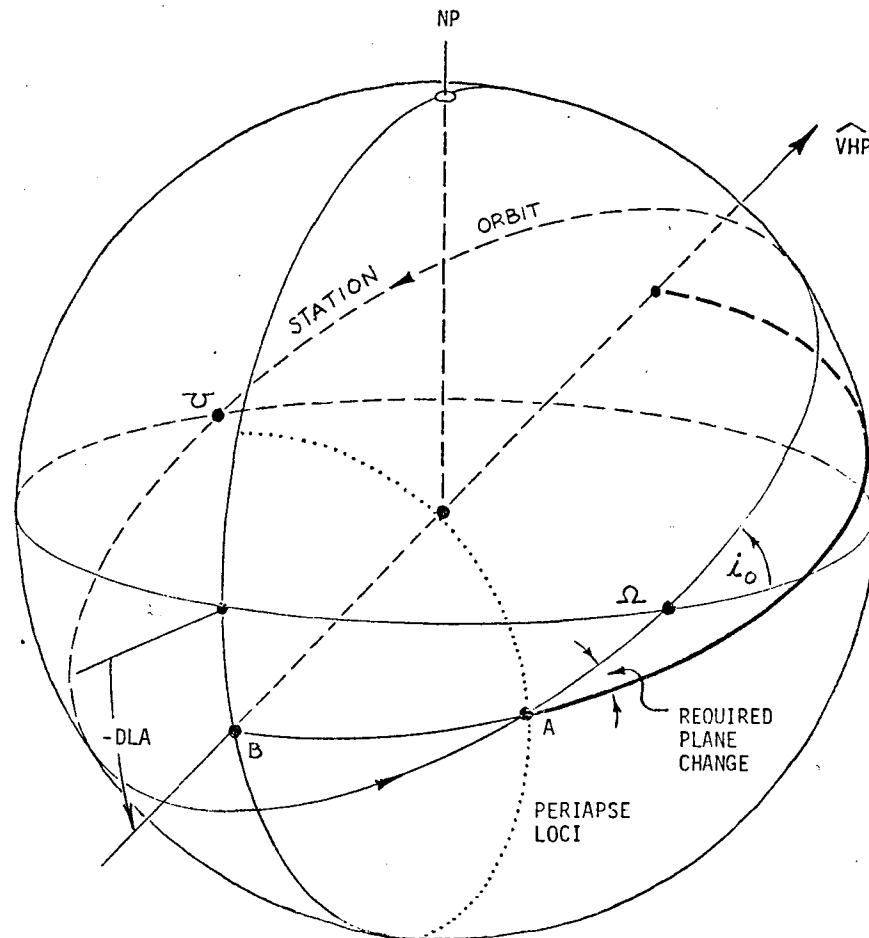
ORBIT ALTITUDE = 200 NM  
 INCLINATION = 28.3 DEG  
 PRECESSION = 7.2 DEG/DAY



LAUNCH TIMING EFFECT OF SPACE STATION ORBIT PRECESSION



CASE A  
OPTIMUM STATION ORBIT ORIENTATION



CASE B  
OFF-OPTIMUM STATION ORBIT ORIENTATION  
(COMBINED MANEUVER STRATEGY SHOWN)

NOTE:  $DLA < i_0$   
A  $\equiv$  ESCAPE IMPULSE POINT

## SPACE STATION/PLANETARY INJECTION STRATEGIES

### UTILIZATION PRIORITIES

- ACTIVE (PROPULSIVE PLANE CHANGES)

- EARTH-ORBITAL

- SPLIT MANEUVER
    - COMBINED MANEUVER
    - THREE-IMPULSE MANEUVER

AS NEEDED FOR DLA TARGETING & LAUNCH DELAYS

- STATION ORBIT REALIGNMENT: EXPENSIVE
    - NON-PLANAR ESCAPE: LESS EXPENSIVE
    - APOAPSE PLANE CHANGE: LEAST EXPENSIVE  
(BUT REQUIRES 24<sup>h</sup> INTERMEDIATE ORBIT)

- INTERPLANETARY

- BROKEN PLANE TRANSFERS

VERY EFFECTIVE ON SOME MISSIONS IN REDUCING DLA PENALTIES AND IN IMPROVING OFF-OPTIMAL ESCAPE REQUIREMENTS FOR PASSIVE STRATEGY (SEE BELOW)

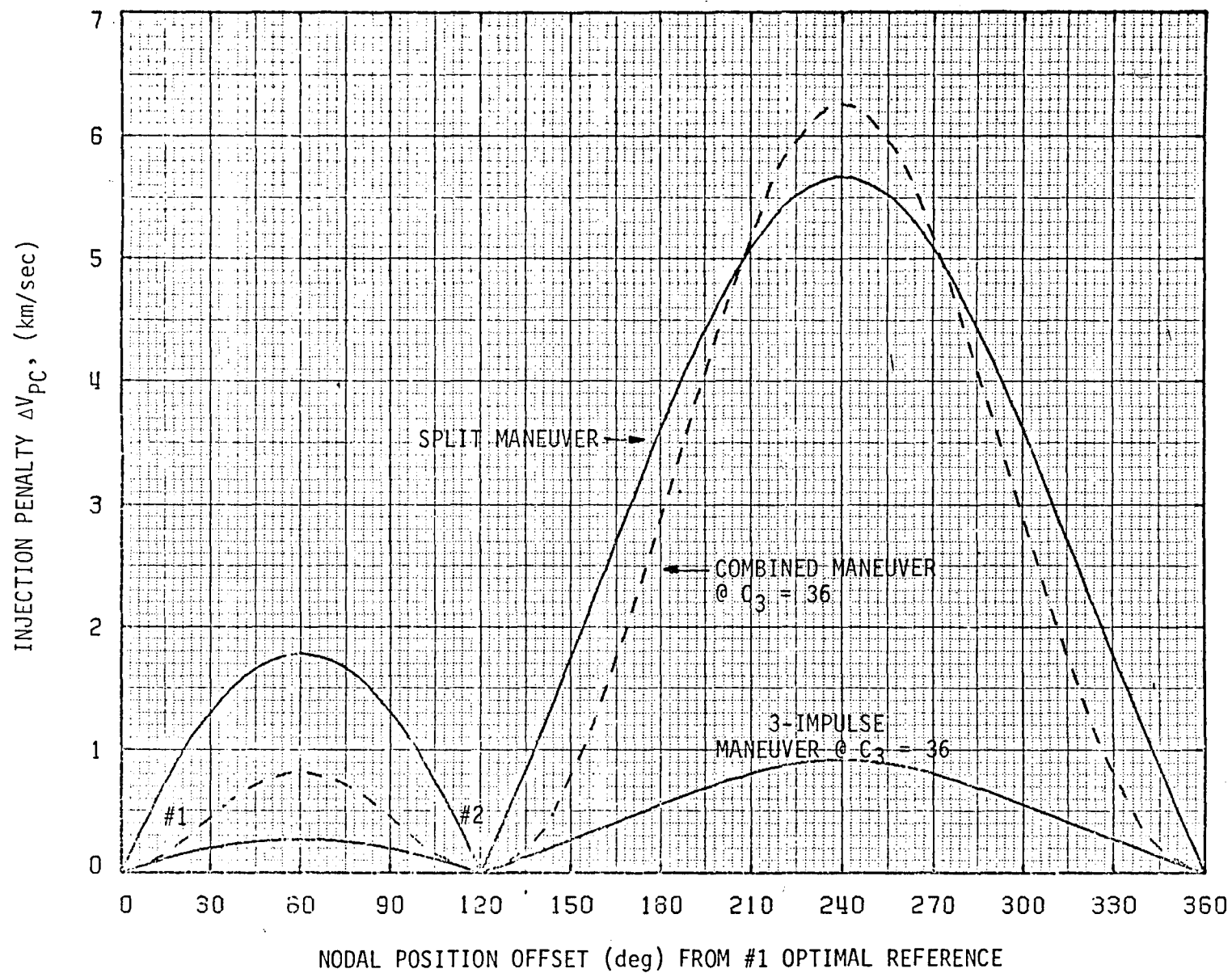
- PASSIVE (LAUNCH DATE TIMING)

- STATION ORBIT PRECESSION

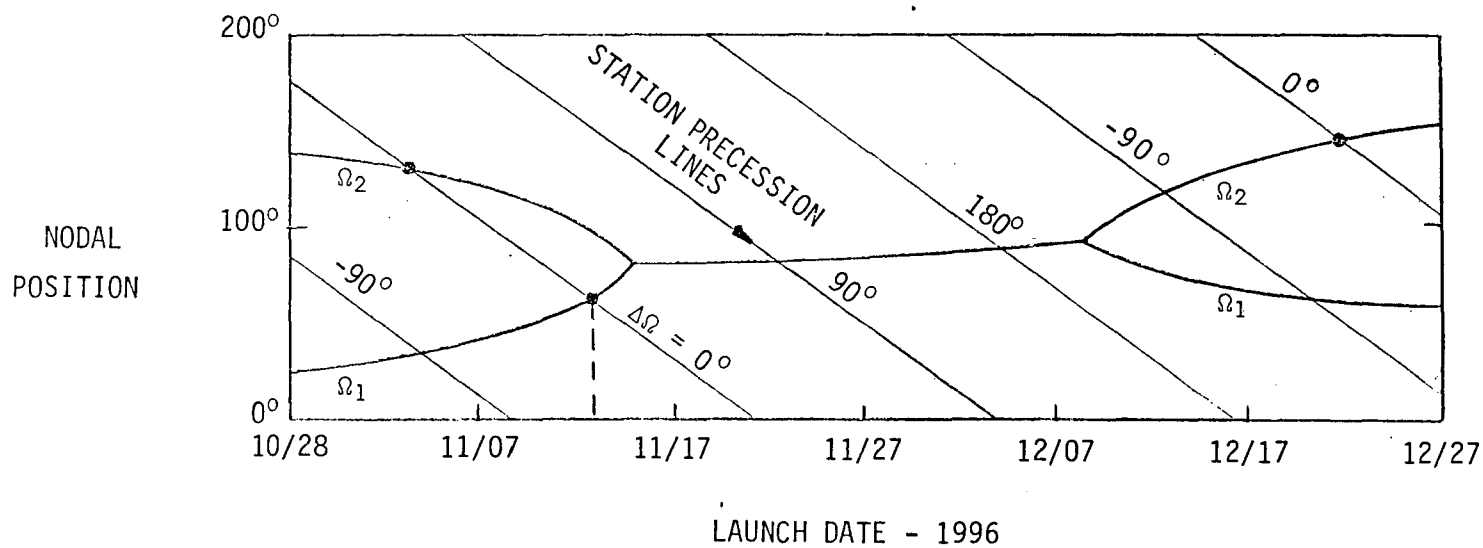
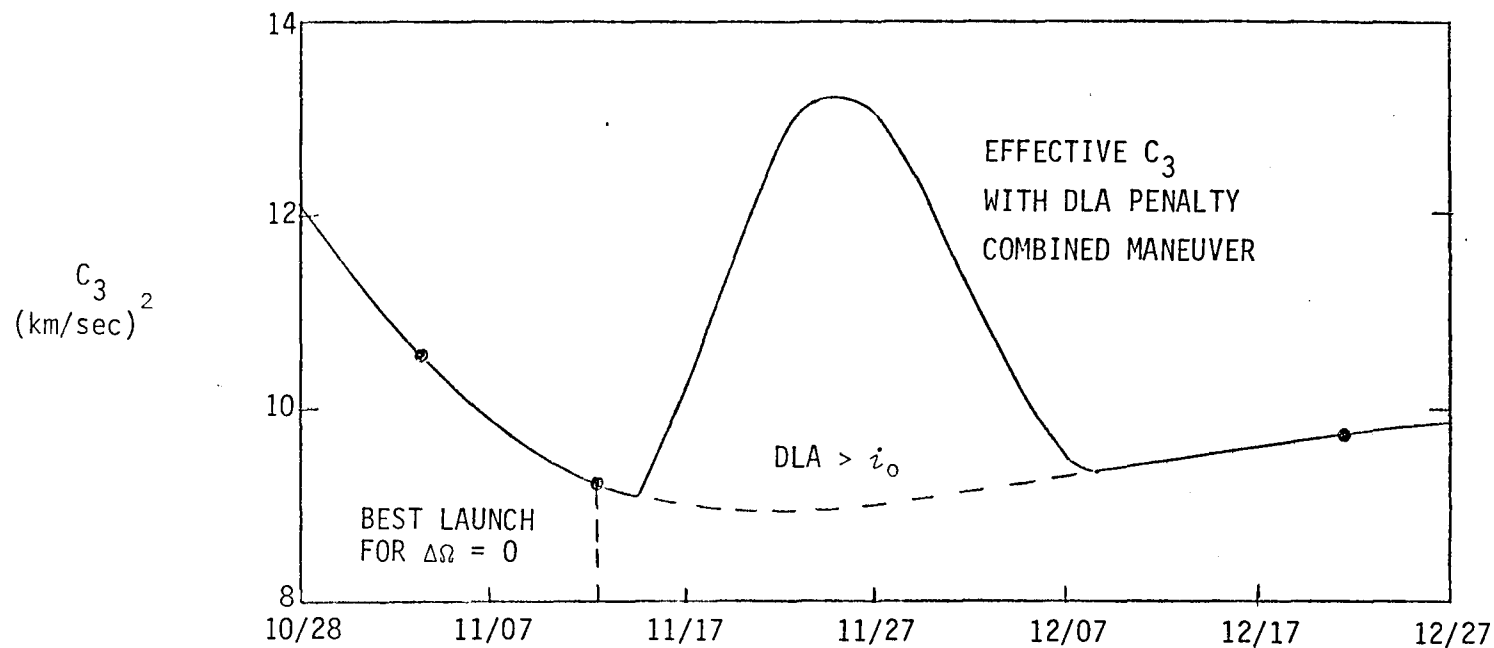
BASELINE SOLUTION

WAITS FOR ORBIT REALIGNMENT, ACCEPTING SOME PERFORMANCE LOSS FROM RESULTING OFF-OPTIMAL LAUNCH DATE

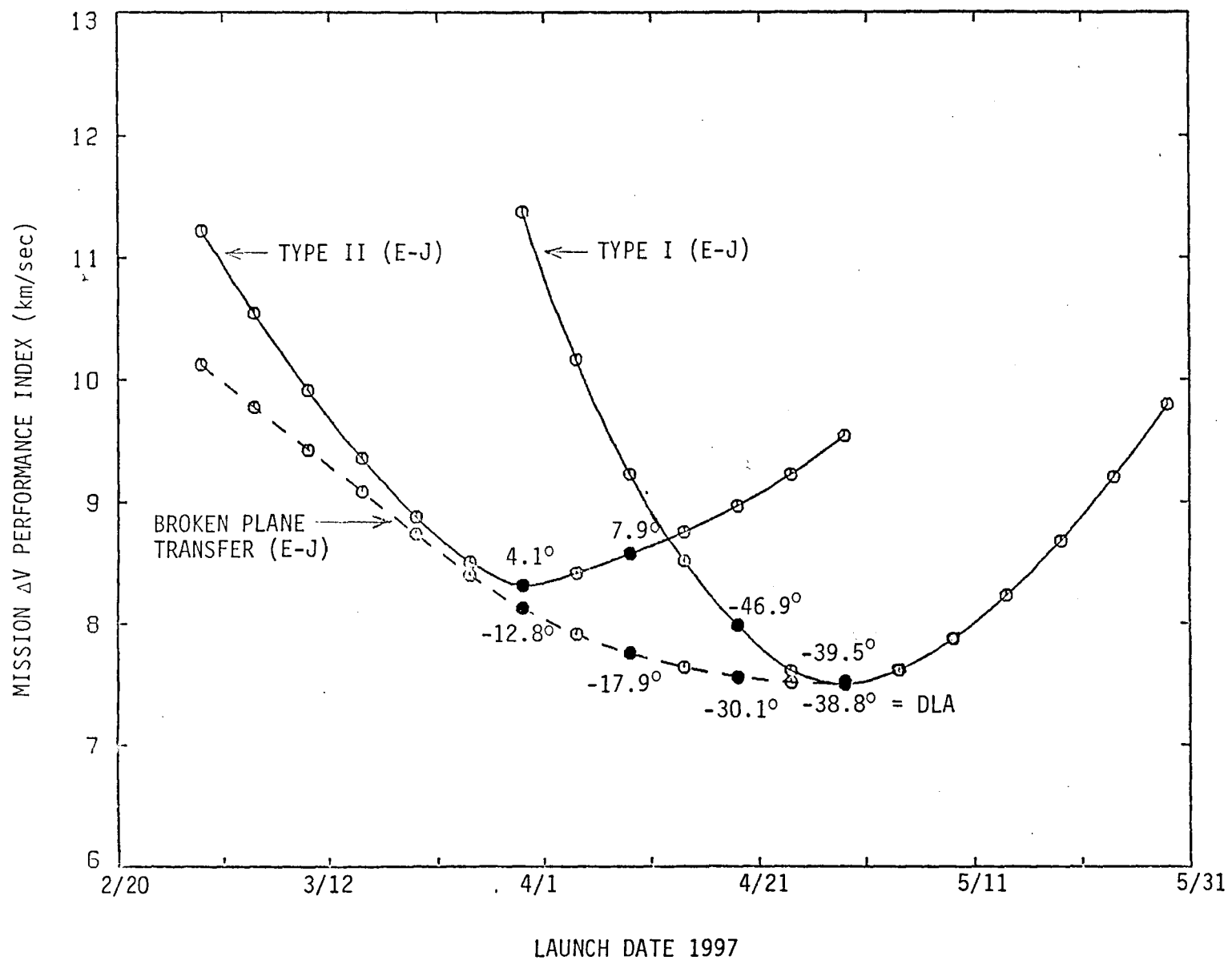




STATION ORBIT INJECTION TO  $|DLA| = 15^\circ$  WITH CORRECTION OF NODAL POSITION OFFSET



SELECTION OF LAUNCH DATE VIA PRECESSION - 1996 MARS SAMPLE RETURN



ADVANTAGE OF BROKEN-PLANE TRANSFERS - 1997 J/S SATURN ORBITER/PROBE MISSION

EXAMPLE  
RESULTS

## CHARACTERISTICS OF EXAMPLE MISSIONS

| <u>MISSION</u>               | <u>LAUNCH YEAR</u> | <u>FLIGHT MODE/OPTION</u>                  | <u>NOMINAL PAYLOAD*</u>                               | <u>COMMENTS</u>                                 |
|------------------------------|--------------------|--|---|---|
| MARS GEOCHEMICAL ORBITER     | 1992               | 300km CIRCULAR ORBIT                       | 505 KG  | $T_F = 0.9^y$                                   |
| MARS SAMPLE RETURN           | 1996               | a) ORBIT RENDEZVOUS<br>b) DIRECT RETURN    | 5 MODULES<br>SEE BREAKDOWN                            | $T_F = 2.7^y$<br>AEROCAPTURE TECH.              |
| MERCURY ORBITER              | 1994               | a) HI-LO ORBITER<br>b) DUAL ORBITERS       | 725 KG IN $12^h$ ORBIT**<br>1050 KG IN $12^h$ ORBIT** | VENUS SWINGBY (2)<br>$T_F = 2.4^y$              |
| ANTEROS RENDEZVOUS           | 1997<br>1999       | a) GOOD OPPORTUNITY<br>b) POOR OPPORTUNITY | 600 KG  | $T_F = 1.2^y$<br>$T_F = 1.1^y$ , HIGH DLA       |
| ASTEROID MULTIPLE RENDEZVOUS | 1992               | MARS SWINGBY                               | 600 KG  | $T_F = 4.5^y$ , 2 TARGETS                       |
| COMET TEMPEL 2 RENDEZVOUS    | 1994               | DIRECT                                     | 600 KG  | $T_F = 5^y$                                     |
| TITAN PROBE                  | 1995               | DIRECT, SATURN FLYBY                       | 250 KG PROBE<br>580 KG BUS                            | $T_F = 3.5^y$                                   |
| URANUS/NEPTUNE PROBES        | 1992               | DIRECT, TANDEM LAUNCH<br>JUPITER SWINGBY   | 235 KG PROBE (x2)<br>560 KG BUS (x2)                  | $T_F = 6.7^y$<br>$T_F = 10^y$                   |
| SATURN ORBITER/PROBE         | 1997<br>1998       | a) FAIR J/S OPP.<br>b) GOOD J/S OPP.       | 250 KG PROBE<br>650 KG ORBITER                        | $T_{FU} = 5.5^y$ , HIGH DLA<br>$T_{FU} = 5.5^y$ |
| GANYMEDE ORBITER             | 2000               | DIRECT                                     | 650 KG  | $T_F = 3.5 - 4.3^y$ WITH<br>SATELLITE G/A TOUR  |

\*NET SPACECRAFT MASS EXCLUDING PROPULSION

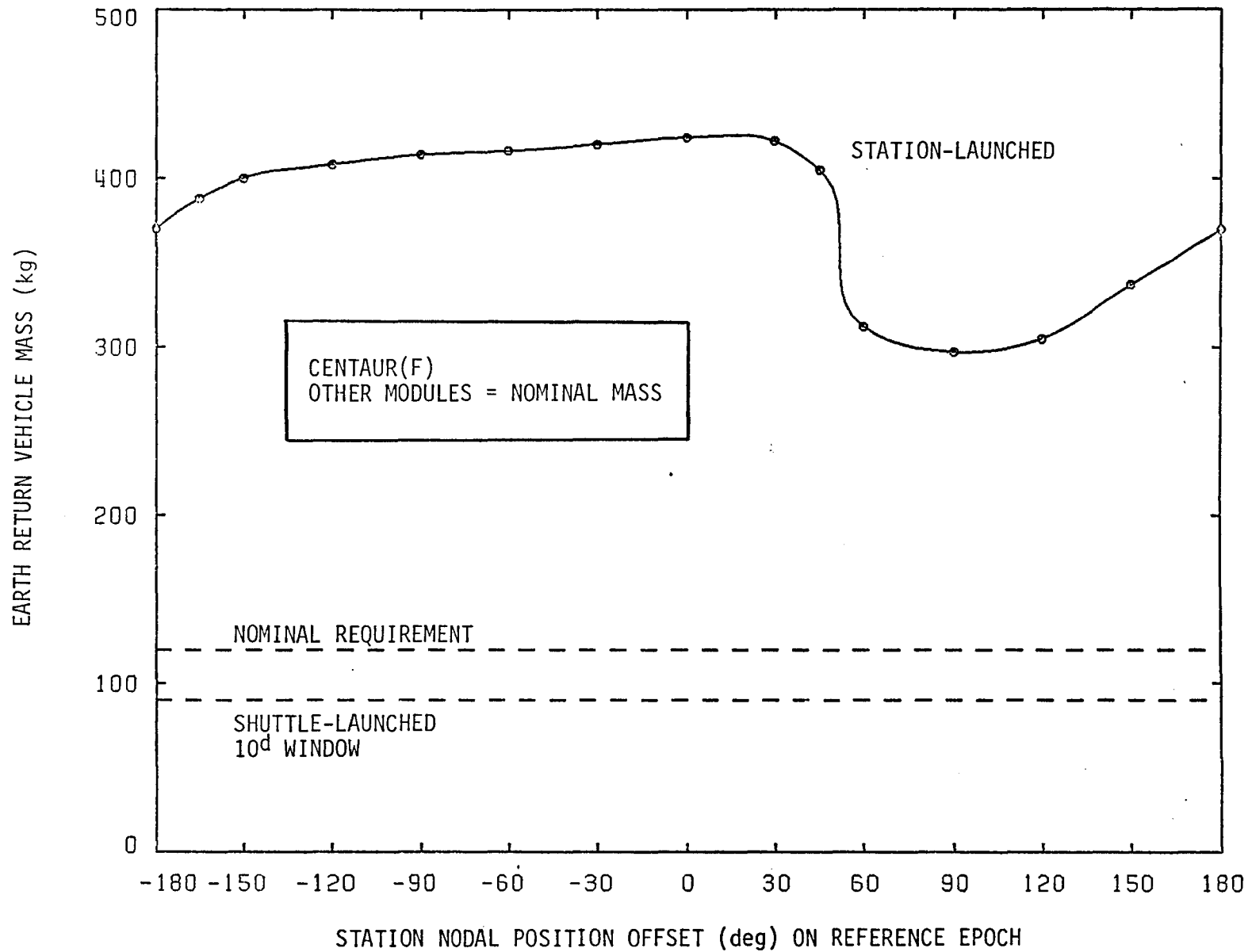
\*\*MERCURY ORBITERS INCLUDES PROPULSION FOR CIRCULARIZATION

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# 1996 MARS SAMPLE RETURN MISSION - MASS DEFINITION

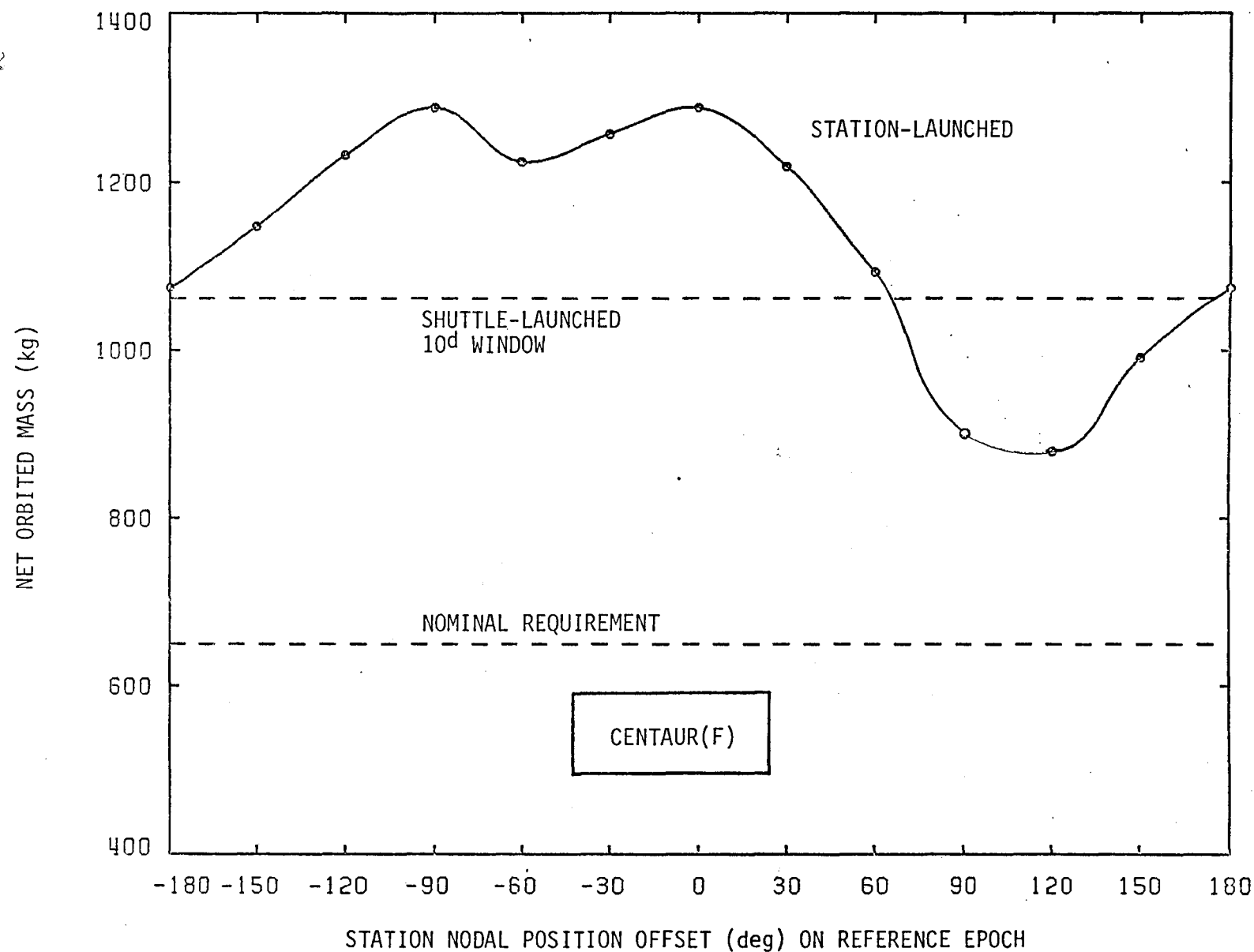
| SYSTEM MASS ELEMENT                                       | - - - NOMINAL VALUE (KG) - - - |                 |
|---|--------------------------------|-----------------|
|   | <u>DIRECT RETURN MODE</u>      | <u>MOR MODE</u> |
| AEROCAPTURE/ENTRY   | 1500                           | 1500            |
| ORBITER   | -                              | 550             |
| LANDER (W/ROVER)  | 650                            | 650             |
| ASCENT VEHICLE SUBSYSTEMS                                 | -                              | 95              |
| EARTH RETURN VEHICLE                                      | 120                            | -               |
| SAMPLE CAPSULE  | 30                             | 30              |
| SAMPLE  | <u>5</u>                       | <u>5</u>        |
| SUBTOTAL W/O PROPULSION                                   | 2305                           | 2830            |
| -----   |                                |                 |
| INJECTED MASS REQUIREMENT                                 |                                |                 |
| SHUTTLE-LAUNCHED  | 8320                           | 5555            |
| STATION-LAUNCHED*   | 8345 - 9085                    | 5515 - 5910     |
| -----   |                                |                 |
| *RANGE OVER ALL POSSIBLE NODAL POSITIONS OF SPACE STATION |                                |                 |

REFERENCE EPOCH = 15 NOV 1996  
OPTIMAL LAUNCH TIMING STRATEGY



PERFORMANCE COMPARISON FOR 1996 MARS SAMPLE RETURN - DIRECT RETURN MODE

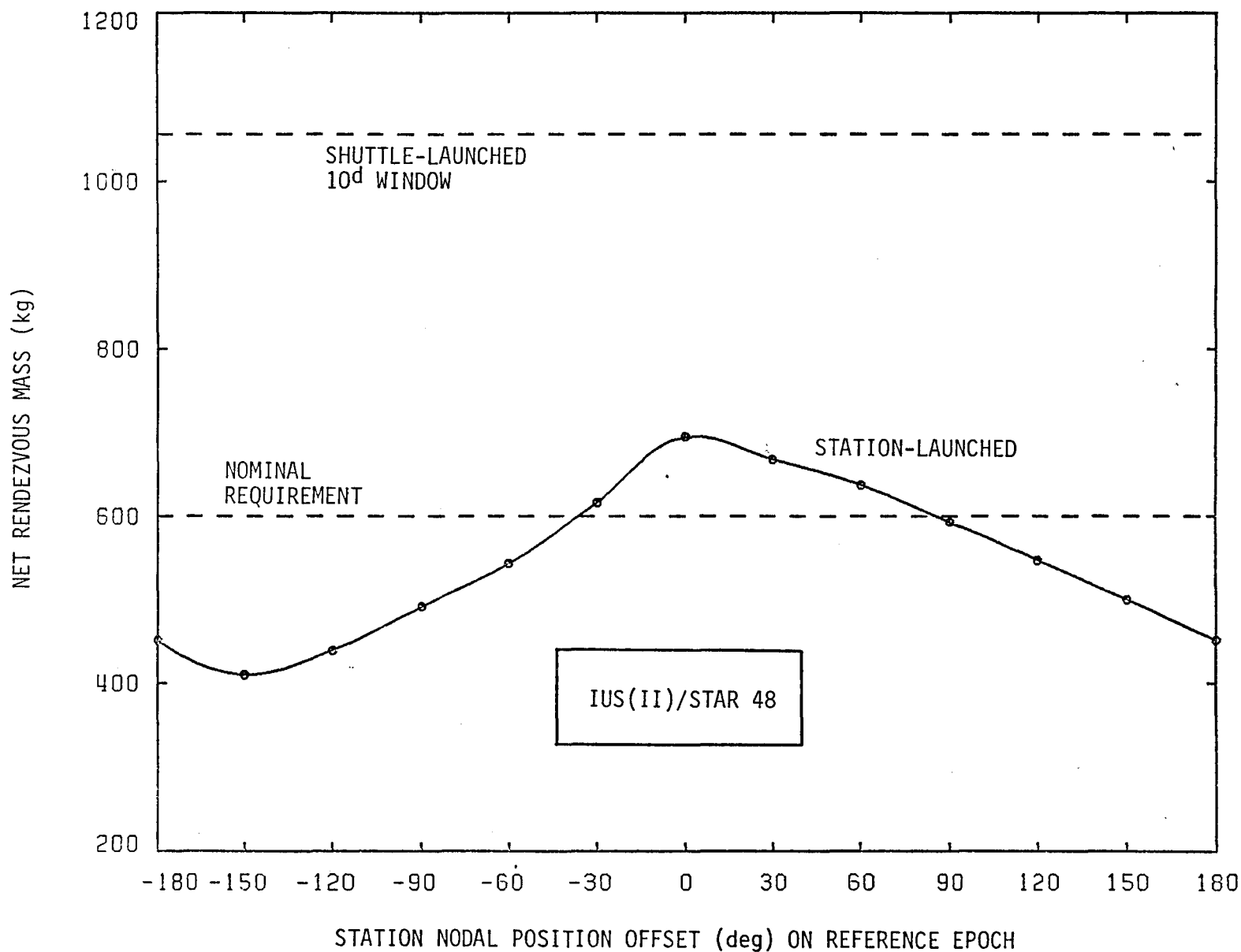
REFERENCE EPOCH = 28 MAY 1998  
OPTIMAL LAUNCH TIMING & BROKEN PLANE STRATEGY



PERFORMANCE COMPARISON FOR 1998 J/S SATURN ORBITER (250 KG PROBE)

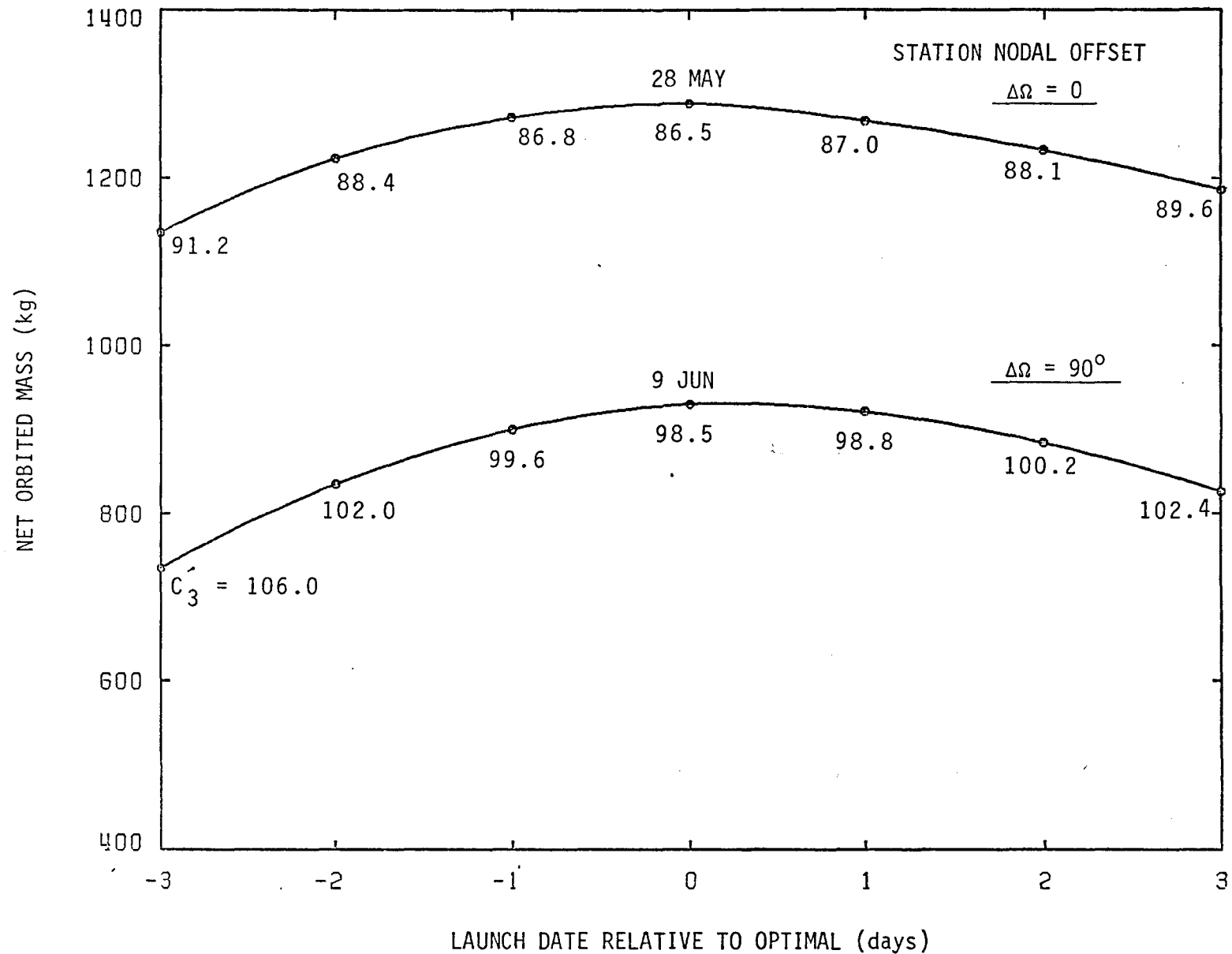


REFERENCE EPOCH = 30 JUN 1999  
OPTIMAL LAUNCH TIMING & BROKEN PLANE STRATEGY



PERFORMANCE COMPARISON FOR 1999 ANTEROS RENDEZVOUS

# CENTAUR(F) PERFORMANCE



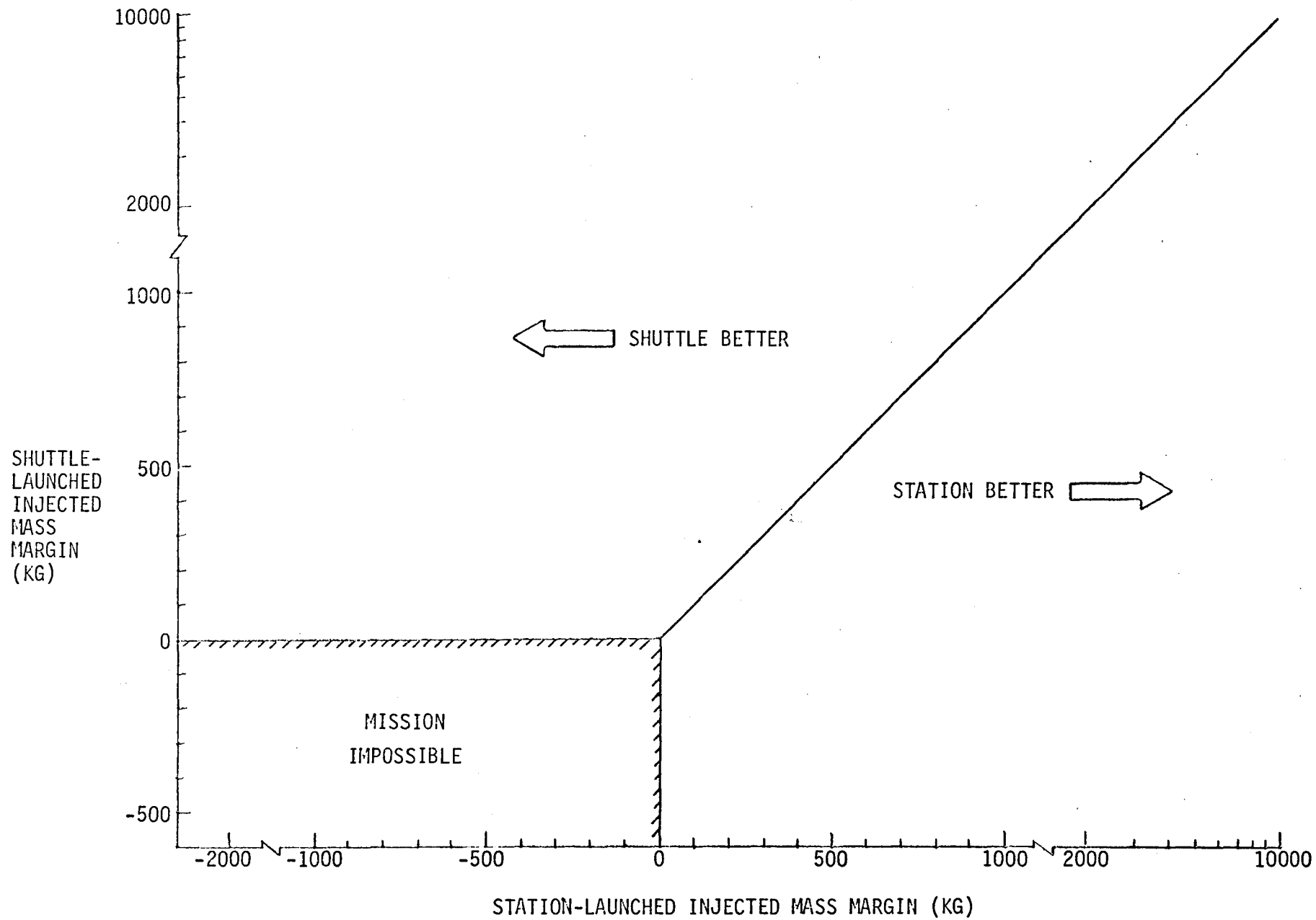
LAUNCH ON-TIME PENALTY - 1998 J/S SATURN ORBITER/PROBE MISSION

SUMMARY  
OF RESULTS

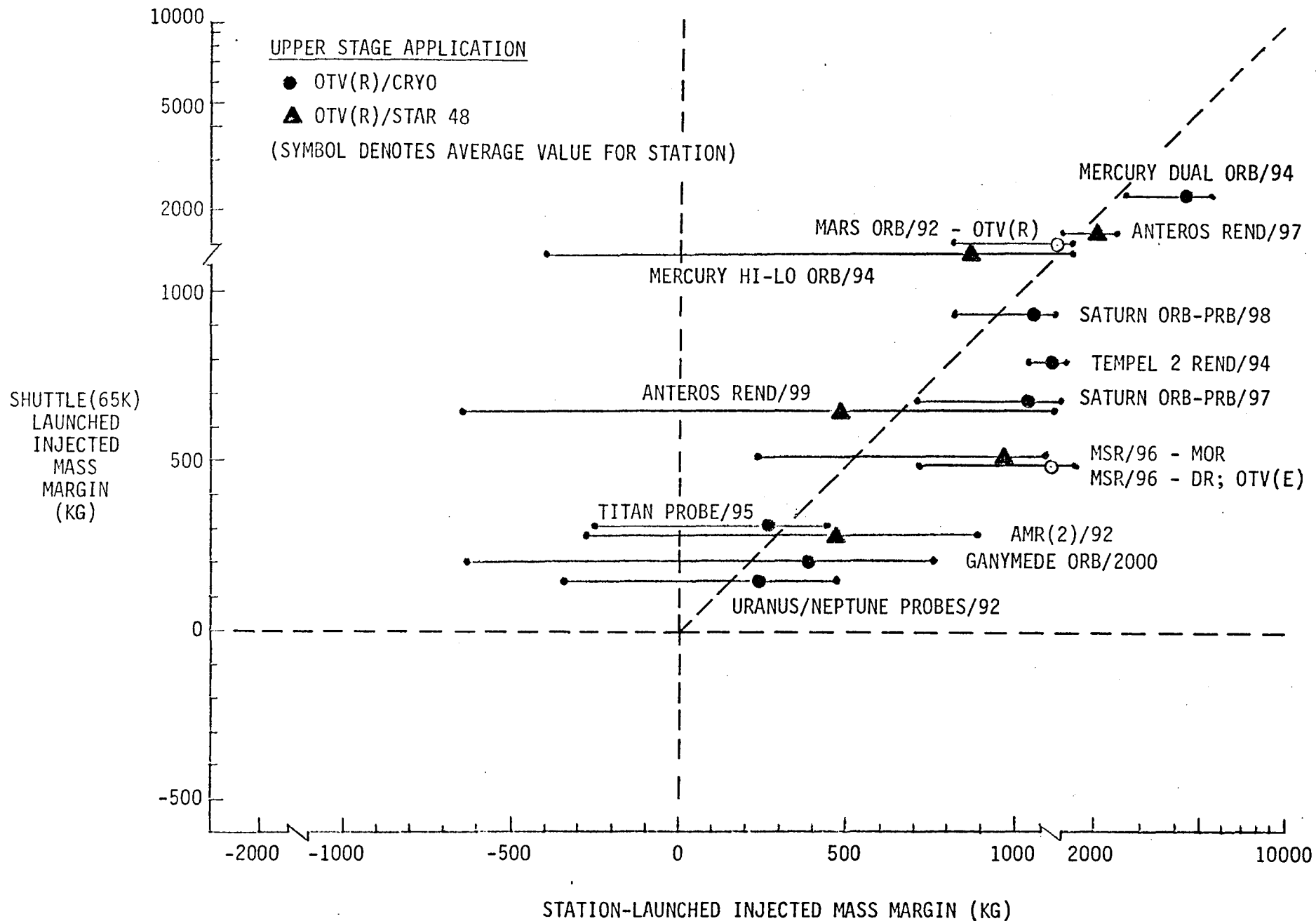
## CRITERIA FOR PERFORMANCE COMPARISON

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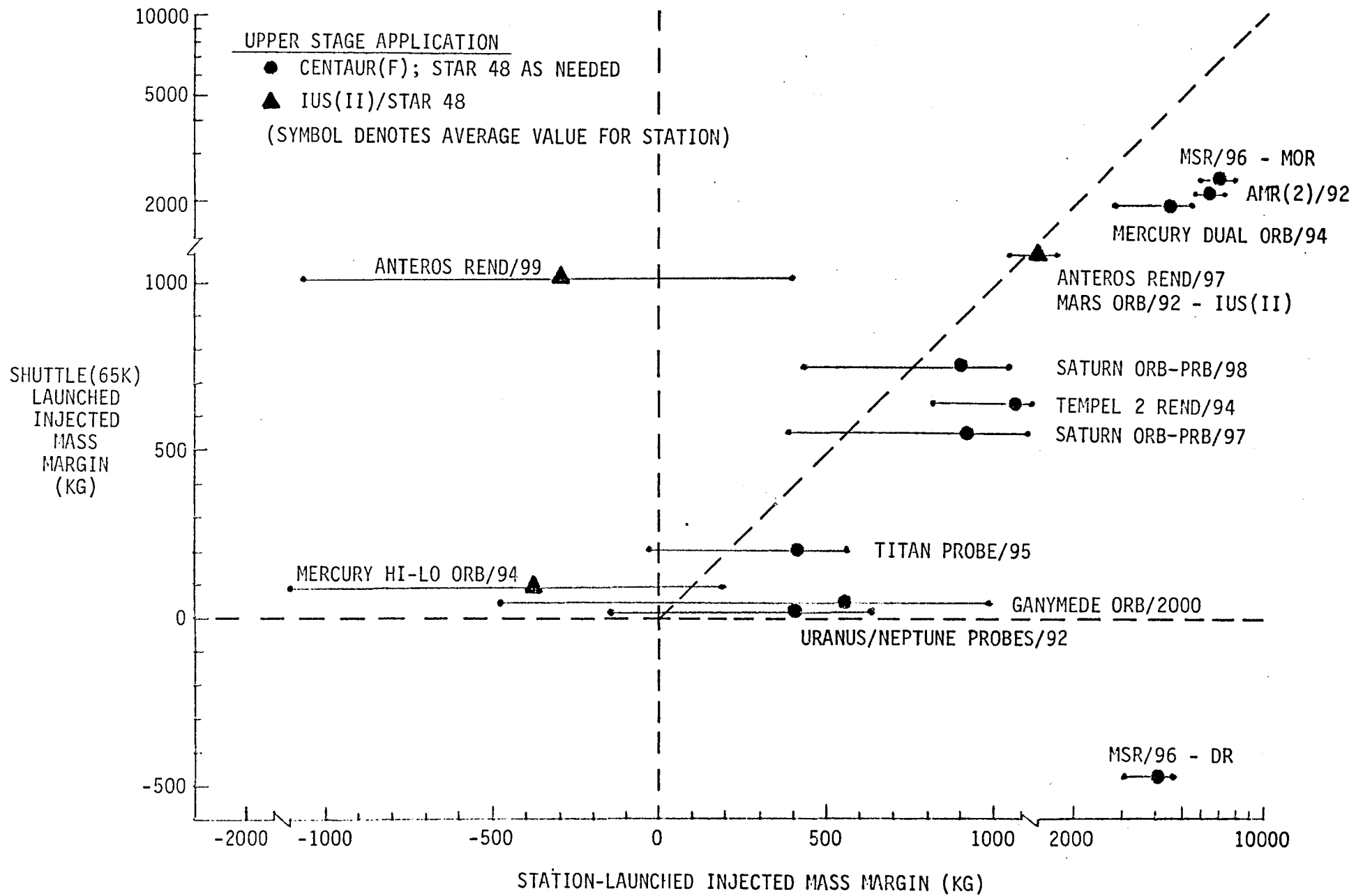
- FOR SPECIFIED NOMINAL PAYLOAD MASS, EXPRESS PERFORMANCE IN TERMS OF INJECTED MASS MARGIN. POSITIVE MARGIN IS MEASURE OF 'SAFETY' OR PAYLOAD GROWTH.
- FOR EACH MISSION, SELECT MINIMUM CAPABILITY UPPER STAGE THAT CAPTURES MISSION WITH SHUTTLE LAUNCH. IF MISSION CANNOT BE CAPTURED, SELECT MAXIMUM CAPABILITY STAGE.
- APPLY SAME UPPER STAGE FOR STATION-LAUNCHED MISSION.
- SHUTTLE LAUNCH WINDOW = 10 DAYS  
STATION LAUNCH WINDOW  $\equiv$  360° OF ALL POSSIBLE NODAL POSITIONS



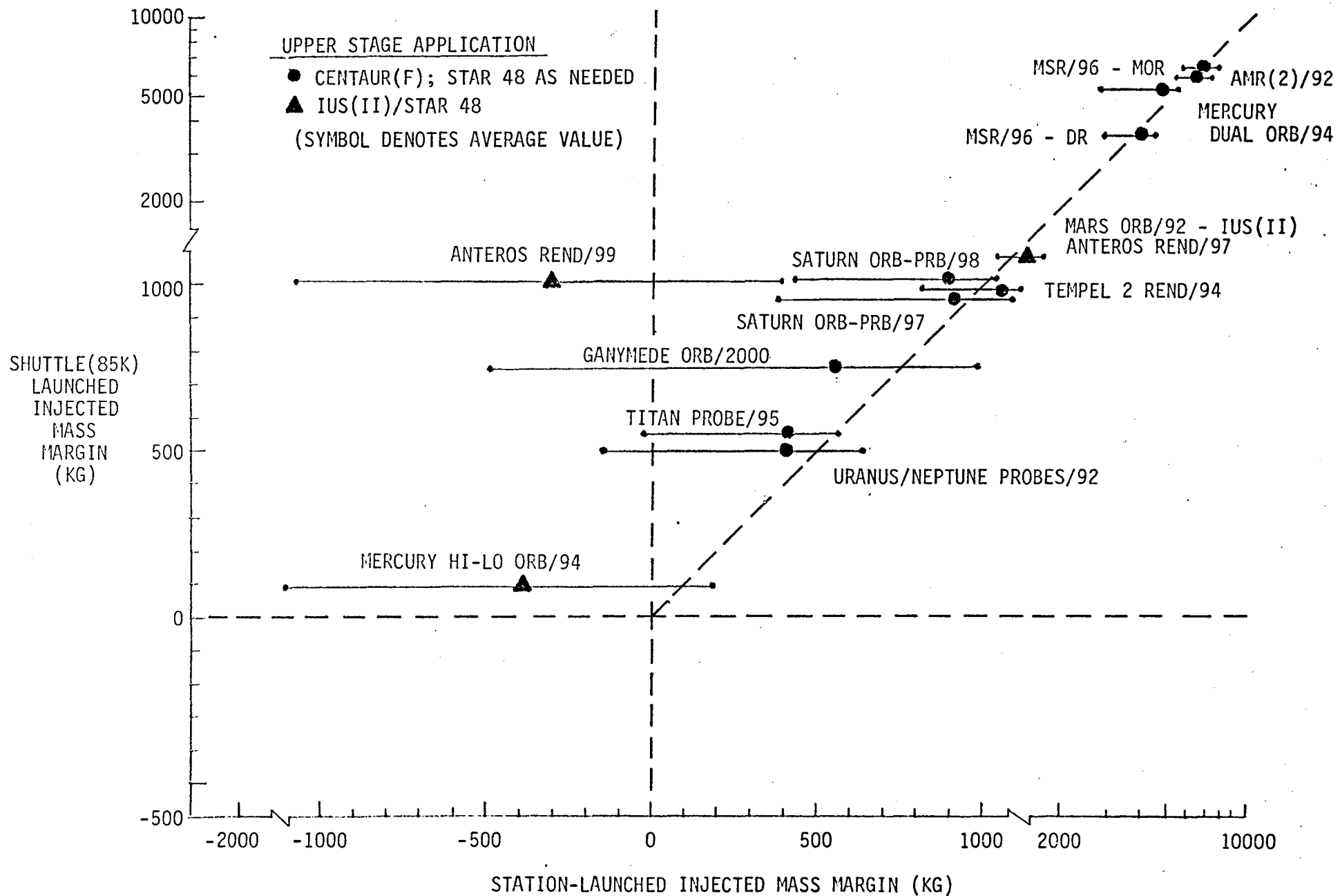
COMPARISON OF SHUTTLE AND SPACE STATION LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE(65K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE(65K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE(85K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE



## CONCLUSIONS

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- A FUNDAMENTAL TRADE-OFF EXISTS BETWEEN SHUTTLE-LAUNCHED AND STATION-LAUNCHED PLANETARY MISSIONS:
  - SHUTTLE LAUNCHES ARE FAVORED BY A MORE ADAPTIVE LAUNCH SITUATION WHICH, FOR A PROPELLANT-FIXED UPPER STAGE, WILL PRODUCE (ON AVERAGE) BETTER PAYLOAD PERFORMANCE
  - STATION LAUNCHES ARE FAVORED BY FREEDOM FROM STAGE PROPELLANT OFF-LOADING DUE TO SHUTTLE CARGO MASS CONSTRAINTS (WHICH MAY PRODUCE BETTER PERFORMANCE), AND BY AN ASSUMED LAUNCH-ON-TIME CAPABILITY
- FOR A BROAD RANGE OF MISSIONS, THESE TRADE-OFFS TEND TO FAVOR:
  - THE SHUTTLE FOR SMALLER PAYLOAD MISSIONS IMPLEMENTED WITH SMALLER UPPER STAGES (e.g. THE IUS(II))
  - THE SPACE STATION FOR LARGER PAYLOAD MISSIONS IMPLEMENTED WITH LARGER UPPER STAGES (e.g. THE WIDE-BODY CENTAUR) OR SPACE-BASED REUSABLE OTV'S
  - ASSUMING A 65K SHUTTLE, THE STATION IS ENABLING ONLY IN A NARROW SENSE FOR SOME MISSIONS (e.g. MSR-DIRECT RETURN MODE). FOR MOST MISSIONS OF INTEREST THE PAYLOAD MARGINS ARE QUITE SUFFICIENT WHETHER SHUTTLE OR STATION LAUNCHED.
- GIVEN THE AVAILABILITY OF AN UPRATED SHUTTLE (e.g. 85K), THE STATION OFFERS NO SIGNIFICANT PAYLOAD DELIVERY BENEFIT. THE ADVANTAGE SHIFTS SLIGHTLY IN FAVOR OF SHUTTLE-LAUNCHED MISSIONS.
- IN SUMMARY, PLANETARY MISSIONS CAN BE LAUNCHED FROM A SPACE STATION WITH NEITHER SIGNIFICANT PERFORMANCE BENEFIT NOR PENALTY.
- OTHER POTENTIAL NON-PERFORMANCE ADVANTAGES OF SPACE STATION (e.g. SHUTTLE MANIFESTING AND ORBIT CHECK-OUT) WILL BE SENSITIVE TO SPECIFIC DESIGN AND OPERATIONAL CHARACTERISTICS OF THE STATION AND ITS SHUTTLE INTERFACE.

